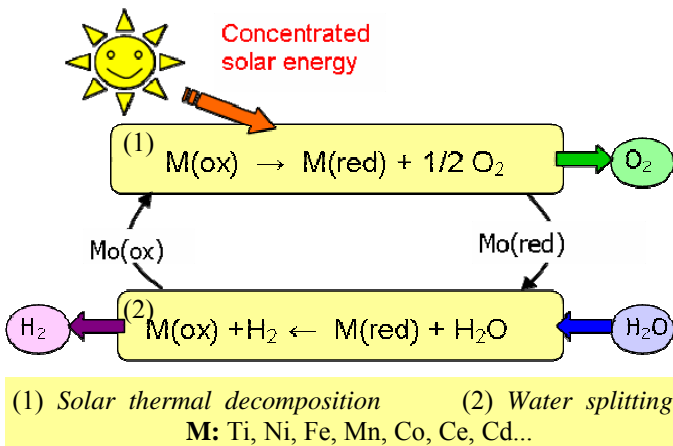


Metal/Metal Oxide cycle

Process Principle



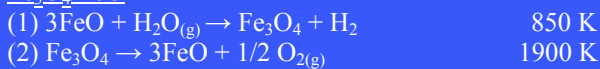
	Reduced	Oxidised	T (K)
Non-volatile metal oxide	Fe ₂ O ₃	Fe ₃ O ₄	1500
	FeO	Fe ₃ O ₄	1900
	Mn ₂ O ₃	MnO	1750-2000
	Co ₃ O ₄	CoO	1600
Volatile metal oxide	CdO	Cd	1750-1800
	CeO ₂	Ce ₂ O ₃	2300

Mo, Sn Ti, Mg, Ca cycles are not mentioned since their reactions occur at temperatures above 2500 K.²

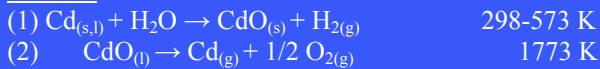
Zn/ZnO cycle is described in another flyer.

TWO-STEP CYCLES

Fe₃O₄/FeO



Cd/CdO

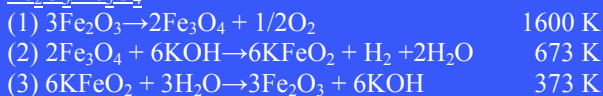


CeO₂/Ce₂O₃

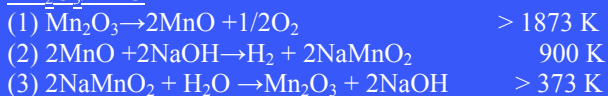


THREE-STEP CYCLES: main cycles

Fe₂O₃/Fe₃O₄



Mn₂O₃/MnO



Advantages:

- H₂ and O₂ gases are removed in separate steps (no high temperature separation step needed),
- No explosive formation gas mixture.¹

Challenges:

- Low efficiency (irreversibility and transfer between stages),
- Low energy yields.¹

Metal/Metal Oxide

Process principle:

- Thermal decomposition using solar energy,
- Hydrolysis (water splitting step).

Heat source: Solar¹

Expected efficiency:

- Fe₂O₃/Fe₃O₄: 18.6 %, ³
- Fe₃O₄/FeO: 17.4 %, ³
- Mn₂O₃/MnO: 16-2 %, ¹
- Cd/CdO: 48.3 % (LHV), ⁴
- Ce₂O₃/CeO₂: NA*.

Cost evaluation: (\$/kg H₂)

- Fe₃O₄/Fe₂O₃: 8.4, ³
- Fe₂O₃/FeO: 7.86 to 14.75, ³
- Mn₂O₃/MnO: NA*,
- Cd/CdO: 4.5 in 2015, ^{4,5}
- Ce₂O₃/CeO₂: NA*.

* NA: Not Available

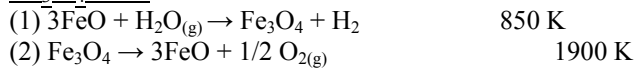


TWO-STEP CYCLES

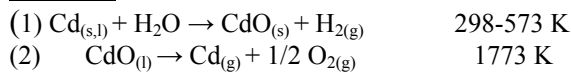
Flow-sheet

The most prominent cycles are:

Fe₃O₄/FeO



Cd/CdO



Hydrolysis (1)

The hydrolysis occurs as steam bubbles through a static pool of molten cadmium.⁴ Hydrolysis efficiency increases in the presence of CO₂.⁶ A quenching step is required to limit oxygen recombination.

Solar thermal decomposition (2)

A window-enclosed decomposer using “beam-down” optics enables the use of inert gas and sub-atmospheric pressure to reduce the decomposition

Description of heat source

Fe₃O₄/FeO

A ferrite reactor (Counter Rotating Ring Receiver Reactor Recuperator) has been designed by SNL¹³. The goal is to use large dish mirrors.

Cd/CdO

A CdO central plant concept solar field has been developed, to permit ground-level operation of all chemical processes using a beam-down collector/

Expected efficiency

Fe₃O₄/FeO

Steinfeld obtained theoretical efficiencies at 61 % at 1900 K to 42 % at 2500 K⁷.

The global efficiency (incorporating all steps from sun to hydrogen) is estimated at 12.7 %⁸ and could

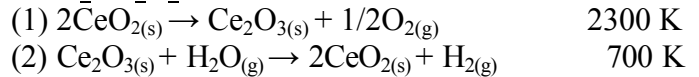
Cost evaluation

Fe₃O₄/FeO

A small size advanced tower plant (32 MW) has been designed to product 100 kg/h of H₂ at \$12.5/kg.⁸ An economic assessment gave hydrogen production cost ranging from \$ 7.98/kg to \$ 14.75/kg of H₂ depending on the level of optimisation considered and on the targeted hydrogen productivity.³

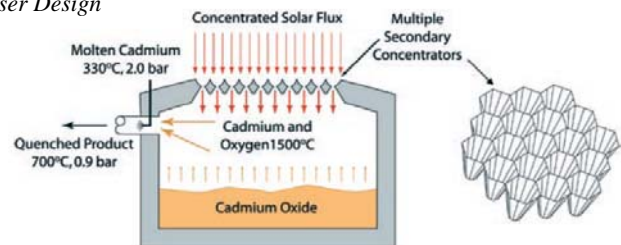
temperature.

-CeO₂/Ce₂O₃



This cycle has never been studied before 2006 but seems to be a promising cycle. Experiments were conducted at lab-scale.²

Schematic of a Beam-Down Multi-Concentrator Cadmium Decomposer Design⁴



concentrator.

A 24-hour hydrogen plant concept was designed. One part of the plant operates under solar radiation, and the second part during solar off-hours with thermally stored energy.⁴

CeO₂/Ce₂O₃

The high temperature needed could be achieved with dish or tower technologies.².

reach 17.4 % in optimized conditions.³

Cd/CdO

In 2008, the DOE project estimated the thermal efficiency at 48.3 % (LHV).⁴

Cd/CdO

H2A analysis leads to an estimated cost range of H₂ /kg of \$3.08 to \$ 4.20.⁵

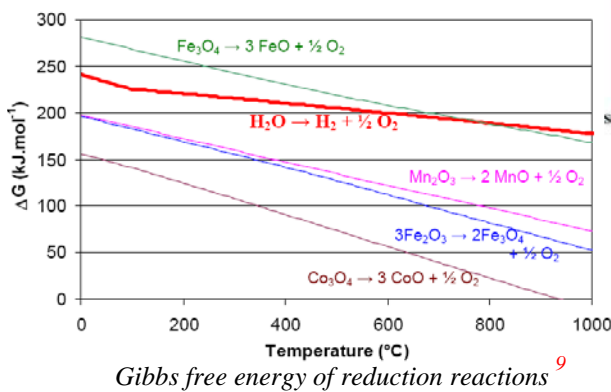
Furthermore, hydrogen plant components have been sized for 100,000 kg/day and the gate-cost based on a 2015 case, was calculated to be around \$ 4.50/kg.⁴



THREE-STEP CYCLES

Flow-sheet

The redox reaction between reduced metal oxide and water is thermodynamically possible only if the Gibbs free energy (G) of the metal oxide redox couple is higher than the G of water reduction. The G curves show that water-splitting is only possible with FeO below 800 °C. MnO, CoO and Fe₃O₄ are not able to split water spontaneously. An additional energy is necessary to run the reaction ($\Delta G > 0$).⁹



The main cycles are:

- 1) Fe₂O₃/Fe₃O₄
 - (1) $3\text{Fe}_2\text{O}_3 \rightarrow 2\text{Fe}_3\text{O}_4 + 1/2\text{O}_2$ 1600 K
 - (2) $2\text{Fe}_3\text{O}_4 + 6\text{KOH} \rightarrow 6\text{KFeO}_2 + \text{H}_2 + 2\text{H}_2\text{O}$ 673 K
 - (3) $6\text{KFeO}_2 + 3\text{H}_2\text{O} \rightarrow 3\text{Fe}_2\text{O}_3 + 6\text{KOH}$ 373 K
- 2) Mn₂O₃/MnO
 - (1) $\text{Mn}_2\text{O}_3 \rightarrow 2\text{MnO} + 1/2\text{O}_2$ > 1873 K
 - (2) $2\text{MnO} + 2\text{NaOH} \rightarrow \text{H}_2 + 2\text{NaMnO}_2$ 900 K
 - (3) $2\text{NaMnO}_2 + \text{H}_2\text{O} \rightarrow \text{Mn}_2\text{O}_3 + 2\text{NaOH}$ > 373 K

Description of heat source

Fe₂O₃/Fe₃O₄: the most suitable concentrating system is a solar tower with a heliostat field (tracking mirrors) in front of the tower.

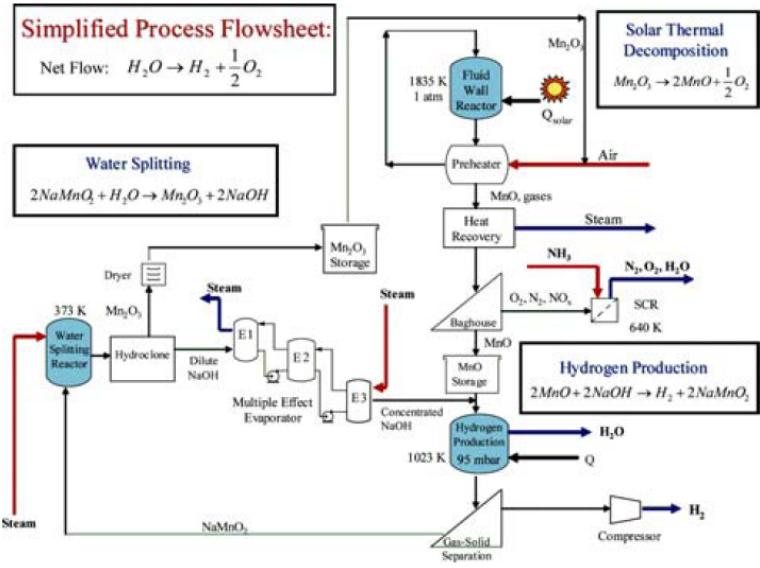
Expected efficiency

Fe₂O₃/Fe₃O₄

The optimized global process efficiency (from solar energy to hydrogen) is estimated to reach 18.6%.¹⁰

Cost evaluation

Fe₂O₃/Fe₃O₄: to produce 250 kg h⁻¹ of hydrogen, the price is 8.4\$/kg with current solar towers.³



Flow-sheet of Mn₂O₃/MnO

The reactants are preheated and fed under pressure into the solar thermal reactor to reach 80 % conversion. The products then pass through four heat exchangers and a filter. The solid stream is sent via a solid conveying system to a storage tank. The gas stream is mixed with NH₃ at 620 K and fed to the selective catalytic reduction system to reduce NO_x. The MnO is mixed with a 50 % NaOH solution and reacts in two rotary furnaces to produce H₂. The vapour is cooled and sent to a series of compressors, heat exchangers and separators. This product, 99.5% H₂ is sent to a hydrogen pipeline. The solid product reacts with water in the third reactor to form Mn₂O₃ which is recycled.¹⁰

Mn₂O₃/MnO: solar energy would be supplied from three 8 MW_{th} heliostat fields¹⁰. H₂ can be produced during off-sun periods (MnO can easily be stored¹¹).

Mn₂O₃/MnO

Sturzenegger and Nuesch calculated efficiencies of 26-51 %, ignoring separation steps, and 16-21% taking all steps into consideration.¹²



IEA/HIA task 25: High Temperature Hydrogen Production Process

Metal/Metal Oxide

Contacts:

- Sabine POITOU, CEA, sabine.poitou@cea.fr
- Gilles FLAMANT, Gilles.Flamant@promes.cnrs.fr

www-prodh2-task25.cea.fr

Main initiatives

SHGR Project (US DOE) –“CR5” reactor.
<http://www.sandia.gov>

France : PROMES-CNRS
<http://www.promes.cnrs.fr>

References

- [1] Perkins C., Weimer A.W., Likely near-term solar-thermal water splitting technologies, *International Journal of Hydrogen Energy*, 29 (2004), pp. 1587 - 1599,
- [2] Abanades S., Flamant G., Thermochemical hydrogen production from a two-step solar-driven water-splitting cycle based on cerium oxides, *Solar Energy*, 80 (2006) pp. 1611-1623,
- [3] Charvin P., Abanades S., Lemort F., Flamant G., Analysis of solar chemical processes for hydrogen production from water splitting thermochemical cycles, *Energy Conversion and Management*, 49 (2008), pp. 1547-1556,
- [4] II.I.1 Development of Solar-Powered Thermochemical Production of Hydrogen from Water, DOE Hydrogen Program, FY 2008 Annual Progress Report,
- [5] Brown L.C., Wong B., Buckingham B., Solar Production of Hydrogen Using a Cadmium Based Thermochemical Cycle, General Atomics, American Institute of Chemical Engineers, November 7th, 2007, Salt Lake City, Utah,
- [6] Brown L.C., McQuillan B., Besenbruch G. E., Solar Production of Hydrogen Using a Cadmium Based Thermochemical Cycle, General Atomics, AIChE Spring Meeting April 26, 2006,
- [7] Steinfeld A., Sanders S., Palumbo R., Design aspects of solar thermochemical engineering. A case study: two-step water-splitting cycle using the Fe₃O₄/FeO redox system, *Solar Energy*, 1999, 65(1) pp. 43-53,
- [8] Charvin P., Hydrogen production via water splitting thermochemical cycles with solar energy water, 2nd SOLLAB Doctorial Colloquium, October 16-18th, 2006,
- [9] Charvin P., Abanades S., Flamant G., Neveu P., Lemort F. Screening and testing of promising solar thermochemical water splitting cycles for hydrogen production, WHEC 16 / 13-16 June 2006 - Lyon France,
- [10] II.I.2 Fundamentals of a Solar-thermal Hydrogen Production Process Using a Metal-Oxide Based Thermochemical Water Splitting Cycle, DOE Hydrogen Program, FY 2006 Annual Progress Report,
- [11] IV.I.2 Fundamentals of a Solar-thermal Mn₂O₃/MnO Thermochemical Cycle to Split Water, DOE Hydrogen Program, FY 2005 Annual Progress Report,
- [12] Sturzenegger M, Nuesch P. Efficiency analysis for a manganese-oxide-based thermochemical cycle, *Energy*, 1999, 24(11) pp. 959-70.
- [13] Diver R., Miller J., Allendorf M., Siegel N. Hogan R. Solar Thermochemical Water-Splitting Ferrite-Cycle Heat Engines, *Journal of Solar Energy Engineering* (2008) Vol. 130 / 041001-1